Power law scaling of lateral deformations with universal Poisson's index for randomly folded thin sheets

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We study the lateral deformations of randomly folded elastoplastic and predominantly plastic thin sheets under the uniaxial and radial compressions. We found that the lateral deformations of cylinders folded from elastoplastic sheets of paper obey a power law behavior with the universal Poisson's index ν =0.17±0.01, which does not depend neither the paper kind and sheet sizes (thickness, edge length) nor the folding confinement ratio. In contrast to this, the lateral deformations of randomly folded predominantly plastic aluminum foils display the linear dependence on the axial compression with the universal Poisson's ratio ν_e =0.33±0.01. This difference is consistent with the difference in fractal topology of randomly folded elastoplastic and predominantly plastic sheets, which is found to belong to different universality classes. The general form of constitutive stress-deformation relations for randomly folded elastoplastic sheets is suggested.

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I. INTRODUCTION

Randomly crumpled thin matter, such as polymerized membranes, biological cells, and thin sheets, is of noteworthy importance for many branches of science and technology. These materials exhibit three distinct phases: the flat, the tubular, and the crumpled (folded).² In the past decade, randomly folded materials become a subject of great interest because of their fascinating topological and mechanical properties.^{3–8} The last are governed by the topology of crumpled configuration.^{8,9} Specifically, the diameter of randomly folded membrane (sheet) is found to scales with the hydrostatic folding force F as $R \propto F^{-\delta,8}$ where the folding force exponent δ is universal and equal to $\delta=3/8$ for phantom and $\delta = 1/4$ for self-avoiding membranes with a finite bending rigidity.⁸ Further, it was found that the statistical topology of randomly folded elastoplastic and predominantly plastic materials are characterized by different sets of universal scaling exponents.⁶

One of the most intriguing mechanical phenomena is that an almost all deformed materials exhibit dimensional changes in lateral directions without corresponding stresses. ¹⁰ This phenomenon, known as Poisson's effect, ^{10,11} may be treated as a particular expression of the Le Chatelier's principle, which states that when a system at equilibrium is subject to a change, the system will respond to relieve the effect of that change. ¹² Indeed, under the equilibrium conditions, the lateral deformations lead to decrease the volume change produced by the applied strains. Specifically, in an axially loaded specimen, Poisson's effect is commonly characterized by the ratio of lateral strain ϵ_{\perp} to axial strain ϵ_{\parallel} , known as Poisson's ratio,

$$\nu_e = -\varepsilon_{\perp}/\varepsilon_{\parallel},\tag{1}$$

which is one of the fundamental physical properties of any natural or engineering material. ¹⁰ In the case of radial compression, the theory of isotropic elasticity predict that

$$\varepsilon_H = -\frac{2\nu_e}{1 - \nu_e} \varepsilon_R,\tag{2}$$

where ε_R and ε_H are the radial and axial strains, respectively.¹³

Although the Le Chatelier's principle implies a positive values of ν_e , such that the Poisson's strains lead to decrease in the relative volume change, a negative Poisson's ratio (that is, a lateral extension in response to stretching) is not forbidden by thermodynamics. 11 In the limit of infinitesimally small strains, the theory of isotropic elasticity allows Poisson's ratios in the range from -1 to 0.5 for threedimensional materials and from -1 to 1 for two-dimensional structures. 13 Materials with $\nu_e = 0$ do not exhibit changes in lateral directions. For most isotropic materials, Poisson's ratio is positive, being close to 0.15 for most ceramics, around of 0.3 for most metals and about of 0.5 for rubbery materials.¹⁰ Generally, the values of Poisson's index and ratio are dependent on the material structure, chemical composition, and porosity. 14,15 However, some classes of materials are characterized by Poisson's ratio or index determined by the material topology. Specifically, Poisson's ratio (index) of elastic fractals is determined by their fractal dimension. 16-18 Materials which expand transversely when stretched longitudinally are called auxetic.¹⁹ The auxetic effect is usually brought about by an in-folding (reentrant) or rotating structure at either the macroscopic or microscopic level.²⁰ Examples of auxetic materials in which a negative Poisson ratio is accounted to their (micro)structure include reentrant foams, crumbled polymerized membranes, fiber networks near the percolation threshold, among others (see Refs. 21-26).

In this way, the auxetic nature of Poisson's effect in the stretching of randomly crumbled paper was demonstrated in Ref. 27 More generally, it was shown that the flat phase of fixed-connectivity membranes provide a wide class of auxetic materials with the universal negative Poisson's ratio $\nu \approx -1/3$, where the symbol \cong denotes the numerical

equality.^{1,26} However, Poisson's effect in the crumpled (folded) phase still remains ununderstood. Accordingly, in this work, we studied Poisson's effect in randomly folded elastoplastic and predominantly plastic thin sheets subjected to the axial and radial compressions.²⁸

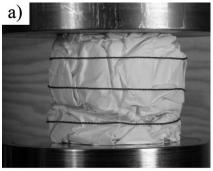
II. EXPERIMENTS AND DISCUSSION

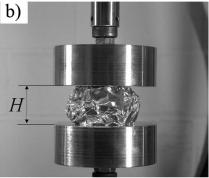
To study Poisson's effect in randomly folded matter in this work, we used five papers of different thicknesses (h =0.024, 0.030, 0.039, 0.068, and 0.087 mm) and bending rigidity, early used in Ref. 6 to study the statistical topology of folded configurations. Square paper sheets with the edge size L of 250, and 500 mm were folded in hands into approximately spherical balls. Then, we confined these balls in cylindrical cells of different diameters to an approximately cylindrical form with the height approximately equal to the diameter. It should be pointed out that once the folding force is withdrawn, the sizes of folded sheet increase logarithmically with time during approximately 1 week due to the strain relaxation (see, for details, Ref. 6). Accordingly, to obtain the cylinders of different dimensions from the sheets of the same size, the folded cylinders were kept in cells under hydrostatic compressions during different times (from 5 min to 48 h) and then relaxed (during 7 days) until no changes in the ball dimensions were observed. Then, the averaged diameter R_0 and height H_0 of each cylinder were determined from 15 random measurements. Thus, we obtained the cylinders with $H_0 \cong R_0$ folded from sheets of the same size L with different contraction ratios $K=L/R_0$, such that $\max K(L)/\min K(L) \ge 2$. In total, 350 folded cylinders were tested under axial compression and 50 under radial compression.

Further, we performed some experiments with randomly folded aluminum foils of thickness 0.02 mm with edge sizes of 200 and 500 mm, the deformations of which are predominantly plastic.⁶ Ten sheets of each size were folded in hands into approximately spherical balls with averaged diameter $R_0 = L/K$ for different contraction ratios.

A. Experiment details

First of all, folded sheets were tested under uniaxial compression in a universal testing machine [see Figs. 1(a) and 1(b)]. The perimeter $P(\lambda_{\parallel}) = 2\pi R$ of deformed cylinder (ball) was measured at different compression ratios $\lambda_{\parallel}=H/H_0$ with the help of silk strings. It should be pointed out that Poisson's ratio is strictly defined only for a small strain linear elastic behavior and it is generally highly strain dependent at larger deformations,²⁹ and even may change the sign.³⁰ Accordingly, in the case of large deformations, the relative lateral expansion/contraction $(\lambda_{\perp} = R/R_0 = P/P_0)$ is commonly described by Poisson's function of axial compression/ stretching $(\lambda_{\parallel}=H/H_0)$, where H_0 , R_0 , and P_0 and H, R, and Pare the specimen height, diameter, and perimeter before and after the deformation, respectively. The form of Poisson's function $\lambda_{\parallel} = f_{\nu}(\lambda_{\parallel})$ is material dependent³¹ and generally, it cannot be characterized by a single parameter, such as Poisson's ratio. However, for some materials, Poisson's function obeys a power law scaling behavior, 16,32





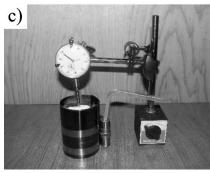


FIG. 1. Experimental setups for tests of [(a) and (b)] uniaxial and (c) radial compressions of [(a) and (c)] randomly folded paper and (b) aluminium foil.

$$\lambda_{\perp} = \lambda_{\parallel}^{-\nu},\tag{3}$$

with the strain independent scaling exponent ν , called Poisson's index, which coincides with Poisson's ratio ν_e only in the limit of infinitesimally small strains, $\varepsilon_{ii} = \sqrt{|\lambda_i^2 - 1|} \ll 1$.

The scaling behavior [Eq. (3)] implies that the mass density $\rho \propto V^{-1}$ of axially deformed material exhibits a fractallike behavior, $\rho \propto \lambda_{\parallel}^{2\nu-1}$. So, the scaling behavior [Eq. (3)] is expected for soft materials with statistically self-similar structures. ^{16,17,32} Early, Gomes *et al.* ³² have reported that the lateral deformations of randomly folded aluminum foils obey the scaling relation [Eq. (3)] with different ν for balls folded from foils of different thicknesses. So, in this work we used the scaling relation [Eq. (3)] to determine Poisson's index.

It should be pointed out that the deformations of folded sheets are essentially irreversible due to the plastic deformations of sheet in the crumpling creases [see Figs. 2(a) and 2(b) and Refs. 4–7]. Moreover, at a fixed compression ratio λ_{\parallel} , the compression stress slowly decreases in time during more than 24 h [see Fig. 2(c) (Ref. 33)]. Generally, the lat-

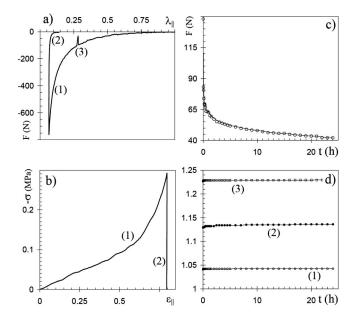


FIG. 2. (a) Typical force (*F*)-compression (λ_{\parallel}) curve of randomly folded paper under the uniaxial compression: (1) loading, (2) unloading, and (3) relaxation shown in (d). (b) Typical stress (megapascals)–strain (arbitrary units) behavior of randomly folded aluminium foil under uniaxial compression: (1) loading and (2) unloading. (c) Compression force *F* (newtons) versus time *t* (hours) for fixed compression ratios λ_{\parallel} =0.5. (d) Lateral expansion ratio λ_{\perp} versus time *t* (hours) for fixed compression ratios λ_{\parallel} =(1) 0.8, (2) 0.5, and (3) 0.3.

eral deformations of viscoelastic materials are also expected to change in time, and so, Poisson's index (ratio) is expected to be time dependent (see Ref. 34). Accordingly, to detect a possible time dependence of Poison's expansion, in the first five experiments performed in this work, the perimeter of deformed cylinder was measured several times for 24 h for each fixed λ_{\parallel} . However, no time dependence in the lateral expansion was noted [see Fig. 2(d) (Ref. 35)].

Additionally, 50 randomly folded paper sheets³⁶ were tested under radial compression in the piston ring compressor [see Fig. 1(b)]. In this case, the axial extension ratio $\lambda_H = H/H_0$ was measured as a function of radial compression ratio $\lambda_R = R/R_0$. Notice that for large deformations, the form of dependence $\lambda_H = F(\lambda_R)$ depends on the form of constitutive equations.

B. Poisson's expansion of randomly folded sheets under uniaxial compression

In Fig. 3(a), the averaged perimeters of axialy deformed cylinders folded with different contraction ratios $K=L/R_0$ ($H_0\cong R_0$) are plotted versus their heights $H=\lambda_\parallel H_0$. One can see that, at least in the range of $0.2\leq \lambda_\parallel \leq 1$, the perimeter scales with H as $P \propto H^{-\nu}$ with the same scaling exponent

$$\nu = 0.17 \pm 0.01$$
 (4)

for all folded sheets tested. Accordingly, Fig. 3(b) shows the data collapse in coordinates λ_{\perp} versus λ_{\parallel} for 350 folded papers sheets tested in this work under uniaxial compression.

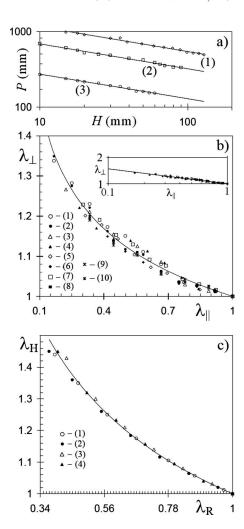


FIG. 3. (a) Perimeter P (millimeters) versus height $H=\lambda_{\parallel}H_0$ for axially compressed cylinders folded from sheets of paper of thickness h=0.039 mm and size L=500 mm with different contraction ratios K=(1) 3.9, (2) 5.6, and (3) 8.3. (b) Lateral expansion ratio λ_{\perp} versus axial compression ratio λ_{\parallel} for all folded paper sheets tested under uniaxial compression; open symbols correspond to cylinders folded from sheets of size 250 mm and full symbols to cylinders folded from sheets of size 500 mm from papers of thickness: [(1) and (2)] 0.024, [(3) and (4)] 0.030, [(5) and (6)] 0.039, [(7) and (8)] 0.068, and [(9) and (10)] 0.087 mm with different contraction ratios; solid line—data fitting with the scaling relations [Eq. (2)] with ν =0.17 (insert shows the same graph plotted in log-log coordinates). (d) Axial expansion ratio λ_H versus radial compression ratio λ_R for radially compressed cylinders folded from sheets of paper of size L=500 mm and thickness of [(1) and (2)] 0.024 and [(3) and (4)] 0.068 mm with contraction ratios (1) and (3) and (2) and (4); symbols—experimental data and solid line—data fitting by the scaling relations [Eq. (4)] with α =0.2.

These data suggest that Poisson's index of randomly folded paper does not depend nether on the environmental conditions (temperature and air humidity³⁷), which were varied in a wide range during 6 months of experiments, nor on the paper thickness, sheet size, and contraction ratio. This finding, together with the universality of local fractal dimension D_l =2.64 ± 0.05,6 suggests the existence of universality class of crumpled phase of randomly folded elastoplastic sheets.

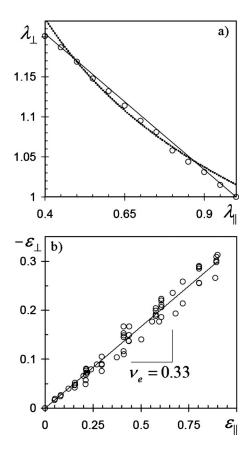


FIG. 4. (a) Lateral expansion ratio λ_{\perp} versus axial compression ratio λ_{\parallel} for randomly folded aluminum foil with size of 500 \times 500 mm²; circles—experimental data, doted line—data fitting with equations [Eq. (3)] with ν =0.22 (R^2 =0.981), and solid line—data fitting with Eq. (1) with ν_e =0.34 (R^2 =0.998). (b) Lateral strains $-\varepsilon_{\perp}$ =[P-P(0)]/P(0) versus axial strains ε_{\parallel} =(R_0 -R)/ R_0 for all aluminum foils tested in this work; solid line—data fitting with ν_e =1/3 (R^2 =0.974).

At the same time, we noted that the universal value [Eq. (4)] differs from values of Poisson's index ν =0.26±0.02 and ν =0.27±0.04, reported in Ref. 32 for randomly folded aluminum foils with thicknesses of 0.007 and 0.037 mm, respectively. So, in this work, we performed 20 experiments with randomly folded aluminum foils with thicknesses of 0.02 mm with edge sizes of 200 and 500 mm. Surprisingly, we noted that while the lateral deformations of randomly folded foils can be fitted by the power-law relation [Eq. (4)] with ν =0.25±0.04 [see Fig. 4(a)], close to the values reported in Ref. 32, the experimental data can be better fitted by the linear relationship [Eq. (1)] with constant Poisson's ratio,

$$\nu_e = 0.33 \pm 0.01,\tag{5}$$

which is found to be independent on the foil size and the folding contraction ratio within a wide range of ε_{\parallel} [see Figs. 4(a) and 4(b)]. The linear relation between lateral and longitudinal strains is quite surprising taking into account that the stress-strain relation is strongly nonlinear for $\varepsilon_{\parallel} \ge 0.5$ [see Fig. 2(b)].

This difference in Poisson's effect, together with the difference in the fractal dimension of randomly folded elastoplastic and predominantly plastic sheets (see Ref. 6), suggests that the randomly folded plastic foils and elastoplastic sheets belong to different universality classes.

C. Radial compression test and general form for constitutive stress-deformation relationship of randomly folded sheets in one- and two-dimensional stress states

In tests with radial compression, we found that the axial extension of randomly folded paper scales with the radial compression as

$$\lambda_H = \lambda_R^{-2\alpha},\tag{6}$$

where the scaling exponent

$$\alpha = 0.20 \pm 0.03 \tag{7}$$

is found to be the same for all tested sheets [see Fig. 3(c)]. So, at least numerically,

$$\alpha \cong \frac{\nu}{1 - \nu},\tag{8}$$

where ν =0.17 ± 0.02 is the universal Poisson's index [Eq. (4)] found in axial compression tests.

The scaling relations [Eqs. (3) and (6)] together with the equality [Eq. (8)] imply that the constitutive stress-deformation relationship of randomly folded sheets should have the following general form:

$$\lambda_i^{-1} = f(\sigma_i) + (\lambda_i \lambda_k)^{\alpha}, \tag{9}$$

where $f(\sigma_i)$ is an increasing function of the principal stress σ_i , such that f(0)=0 and α is defined by relationship;⁵ indexes $i \neq j \neq k$ take values of 1, 2, and 3, corresponding to the direction of principal stress (see Ref. 13).

III. CONCLUSIONS

We found that Poisson's expansion of randomly folded elastoplastic sheets under axial and radial compression displays a power-law scaling behavior with the universal scaling exponent [Eq. (4)], whereas the lateral strains of randomly folded aluminum foils depend linearly on the longitudinal strains within a surprisingly wide range of strains. Poisson's ratio of randomly folded aluminum foils is also universal, i.e., independent on the foil thickness, sheet size, and folding contraction ratio. So, our findings suggest that randomly folded elastoplastic and predominantly plastic sheets belong to different universality classes.

It should be pointed out that the universality of Poisson's index and ratio is very surprising, taking into account that Poisson's ratio of common porous materials (metals, ceramics, polymers, and soils) strongly depends on the porosity (p) or relative mass density $[\rho/\rho_0=(1-p)]$, which in the case

of randomly folded sheets depends on the contraction ratio as $\rho/\rho_0 = K^3$.³⁸

The findings of this work provide an insight into the relation between the topology and mechanical properties of randomly folded matter. We expect that these findings will stimulate the theoretical studies and numerical simulations of Poisson's effect in the crumpled phase of randomly folded thin sheets and polymerized membranes.

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- ³⁸ In the case of randomly folded sheets under hydrostatic compression, the scaling relation $R \propto F^{-\delta}$ with $\delta = 1/4$ (Ref. 8) implies that the bulk modulus scales with the mass density of folded configuration $\rho \propto M/R^3$ as $B \propto R^3 \partial (F/R^2)/\partial R^3 \propto \rho^n \propto (1-p)^n \propto K^{3n}$, with the universal elastic exponent $n = (1+2\delta)/3\delta = 2$.